

Simulation of Surface Chemical Reactions

in a Monolith Channel for Hydrogen Production



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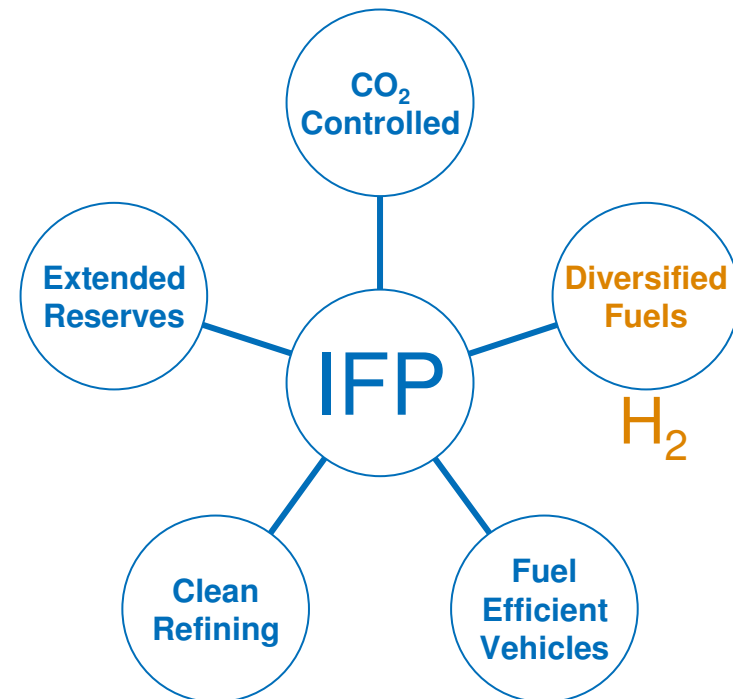
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IFP Presentation

- French R&D public institute
- Mission:
 - To **develop** the technologies and materials of the future in field of **energy, transport** and the **environment**
- Some numbers about IFP:
 - 2 main locations (Rueil and Lyon)
 - ~1800 workers (~1100 researchers)
 - ~200 PhD and post-doctoral students
- More information at: www.IFP.fr

5 strategic priorities



H₂ production from CH₄ by ATR process over monoliths

- In an ATR reactor, three main reactions occurs:

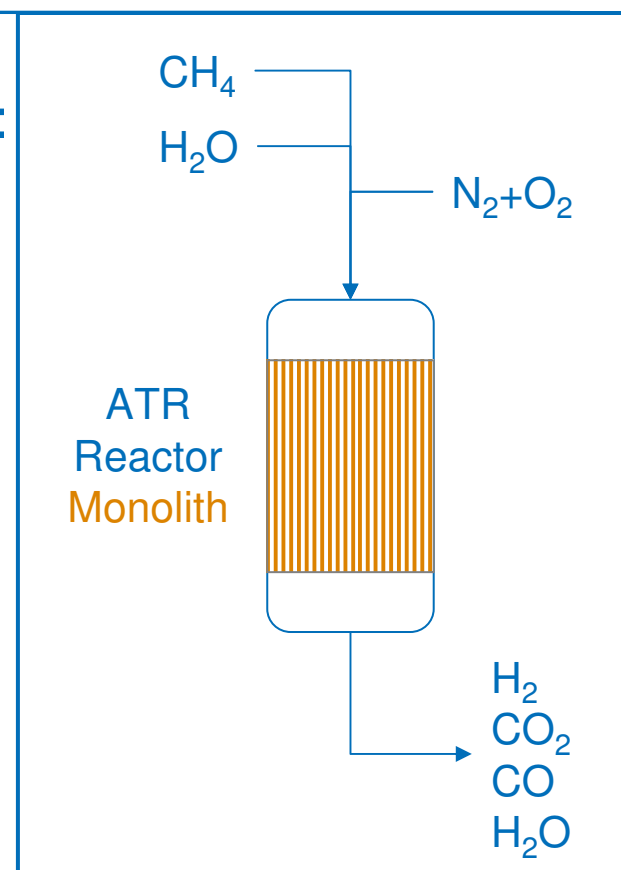


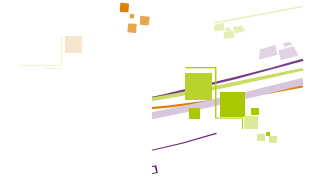
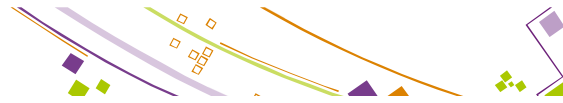
↑
Energy



Thermodynamic
Equilibrium Expected

- This system need to be catalyzed
 - In our case: Impregnated monoliths

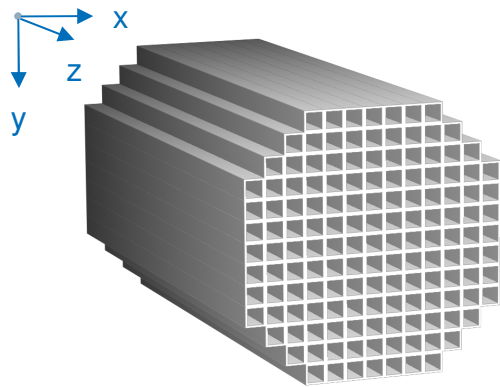




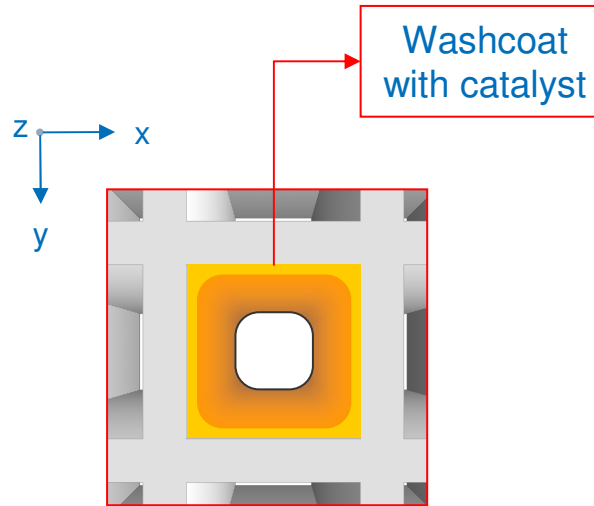
Objectives

- The objective is to build an isothermal reactor model.
- It will be shown:
 - The geometry definition and governing equations
 - Two different approaches to model the catalytic layer
 - The set of 20 mass balance equations
 - Involved with 42 surface chemical reactions
 - The main simulation results
 - The trend evaluations

Problem Definition: Global Geometry



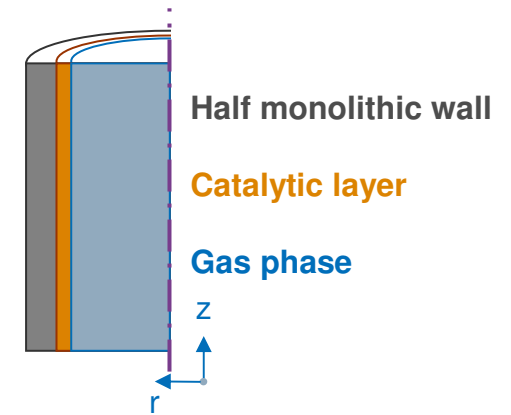
Monolith



Modeling only a channel

Shape between circle
and square
3D

Axial symmetric
geometry



Cylindrical Channel
2D

Problem Definition: Governing Equations

Hydrodynamic:

- Gas phase: Poiseuille profile
- Catalytic layer: No velocity

Masse Balance Equation

$$\frac{\partial C_k}{\partial t} + \nabla \cdot (-D \nabla C_k + C_k u) = R$$

- For 7 Gas Species (H_2 , O_2 , H_2O , CH_4 , CO , CO_2 and N_2)

- Gas Phase - Convection and Diffusion**

$$\frac{\partial C_k}{\partial t} + \nabla \cdot (-D \nabla C_k + C_k u) = 0$$

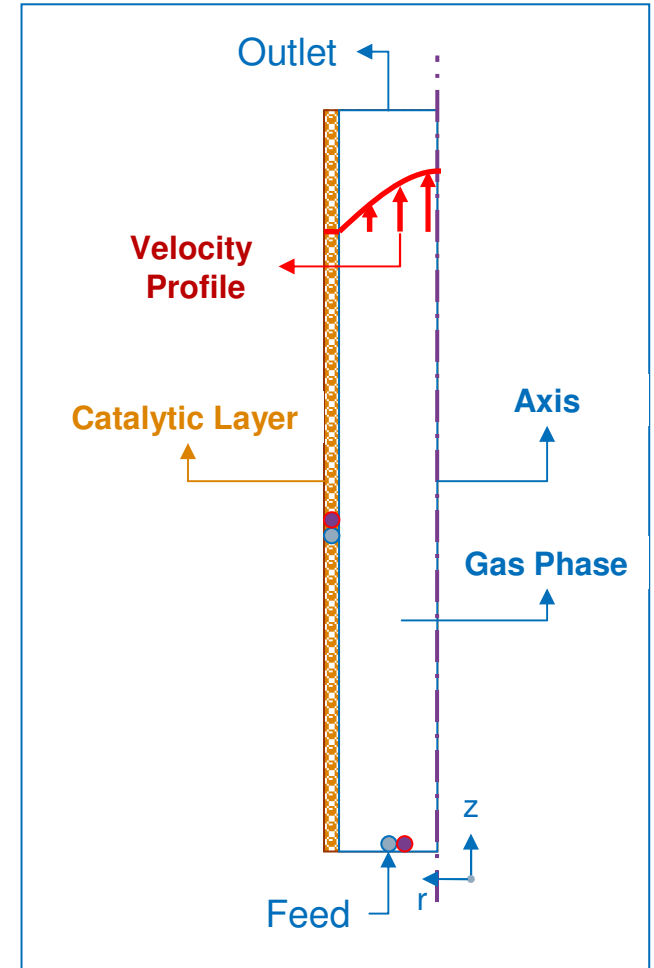
- Catalytic Layer - Diffusion and Surface Reaction**

$$\frac{\partial C_k}{\partial t} + \nabla \cdot (-D \nabla C_k) = R$$

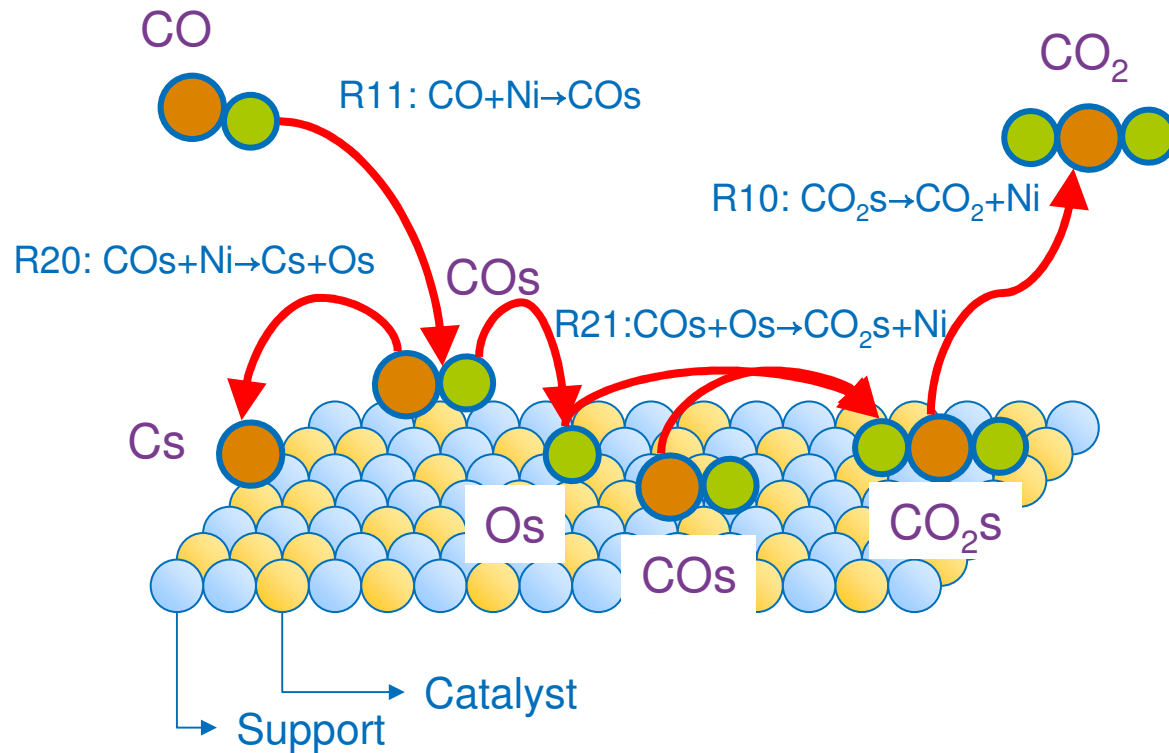
- For 13 adsorbed species (from a surface mechanism)

- Only the surface reactions are taken in count (considering the mean field approximation)

$$\begin{cases} \frac{\partial C_{s_k}}{\partial t} = R, k-1 \\ \text{site balance, } k \end{cases}$$



Problem Definition: Chemical Reaction Mechanism

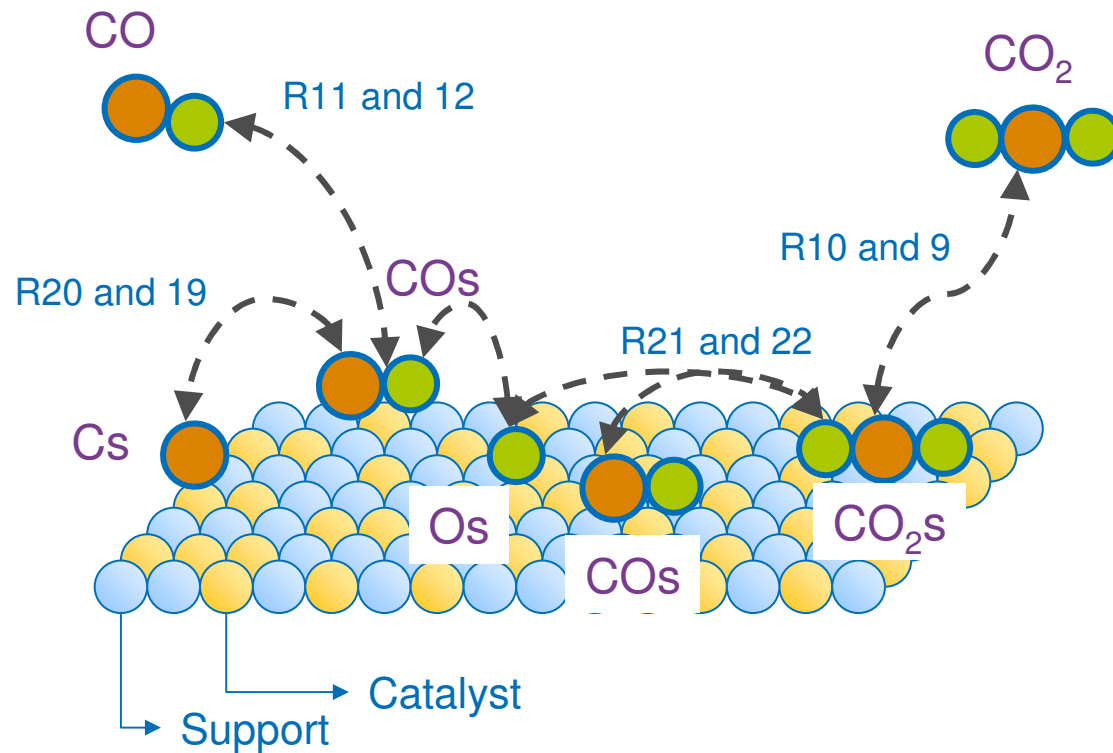


Surface Adsorption/Desorption Reactions

R1	H_2	+	$2\text{Ni}(\text{s})$	\rightarrow	$2\text{H}(\text{s})$		
R2			$2\text{H}(\text{s})$	\rightarrow	H_2	+	$2\text{Ni}(\text{s})$
R3	O_2	+	$2\text{Ni}(\text{s})$	\rightarrow	$2\text{O}(\text{s})$		
R4			$2\text{O}(\text{s})$	\rightarrow	O_2	+	$2\text{Ni}(\text{s})$
R5	CH_4	+	$\text{Ni}(\text{s})$	\rightarrow	$\text{CH}_4(\text{s})$		
R6			$\text{CH}_4(\text{s})$	\rightarrow	CH_4	+	$\text{Ni}(\text{s})$
R7	H_2O	+	$\text{Ni}(\text{s})$	\rightarrow	$\text{H}_2\text{O}(\text{s})$		
R8			$\text{H}_2\text{O}(\text{s})$	\rightarrow	H_2O	+	$\text{Ni}(\text{s})$
R9	CO_2	+	$\text{Ni}(\text{s})$	\rightarrow	$\text{CO}_2(\text{s})$		
R10			$\text{CO}_2(\text{s})$	\rightarrow	CO_2	+	$\text{Ni}(\text{s})$
R11	CO	+	$\text{Ni}(\text{s})$	\rightarrow	$\text{CO}(\text{s})$		
R12			$\text{CO}(\text{s})$	\rightarrow	CO	+	$\text{Ni}(\text{s})$
Surface Reactions (involving O, H and Ni atoms)							
R13	$\text{H}(\text{s})$	+	$\text{O}(\text{s})$	\rightarrow	$\text{Ni}(\text{s})$	+	$\text{OH}(\text{s})$
R14	$\text{Ni}(\text{s})$	+	$\text{OH}(\text{s})$	\rightarrow	$\text{H}(\text{s})$	+	$\text{O}(\text{s})$
R15	$\text{H}(\text{s})$	+	$\text{OH}(\text{s})$	\rightarrow	$\text{Ni}(\text{s})$	+	$\text{H}_2\text{O}(\text{s})$
R16	$\text{Ni}(\text{s})$	+	$\text{H}_2\text{O}(\text{s})$	\rightarrow	$\text{H}(\text{s})$	+	$\text{OH}(\text{s})$
R17			$2\text{OH}(\text{s})$	\rightarrow	$\text{H}_2\text{O}(\text{s})$	+	$\text{O}(\text{s})$
R18	$\text{H}_2\text{O}(\text{s})$	+	$\text{O}(\text{s})$	\rightarrow	$2\text{OH}(\text{s})$		
Surface Reactions (involving O, C and Ni atoms)							
R19	$\text{C}(\text{s})$	+	$\text{O}(\text{s})$	\rightarrow	$\text{Ni}(\text{s})$	+	$\text{CO}(\text{s})$
R20	$\text{Ni}(\text{s})$	+	$\text{CO}(\text{s})$	\rightarrow	$\text{C}(\text{s})$	+	$\text{O}(\text{s})$
R21	$\text{CO}(\text{s})$	+	$\text{O}(\text{s})$	\rightarrow	$\text{Ni}(\text{s})$	+	$\text{CO}_2(\text{s})$
R22	$\text{Ni}(\text{s})$	+	$\text{CO}_2(\text{s})$	\rightarrow	$\text{CO}(\text{s})$	+	$\text{O}(\text{s})$
Surface Reactions (involving C, O, H and Ni atoms)							
R23	$\text{Ni}(\text{s})$	+	$\text{HCO}(\text{s})$	\rightarrow	$\text{H}(\text{s})$	+	$\text{CO}(\text{s})$
R24	$\text{H}(\text{s})$	+	$\text{CO}(\text{s})$	\rightarrow	$\text{Ni}(\text{s})$	+	$\text{HCO}(\text{s})$
R25	$\text{Ni}(\text{s})$	+	$\text{HCO}(\text{s})$	\rightarrow	$\text{CH}(\text{s})$	+	$\text{O}(\text{s})$
R26	$\text{CH}(\text{s})$	+	$\text{O}(\text{s})$	\rightarrow	$\text{Ni}(\text{s})$	+	$\text{HCO}(\text{s})$
Surface Reactions (involving C, H and Ni atoms)							
R27	$\text{Ni}(\text{s})$	+	$\text{CH}_4(\text{s})$	\rightarrow	$\text{H}(\text{s})$	+	$\text{CH}_3(\text{s})$
R28	$\text{H}(\text{s})$	+	$\text{CH}_3(\text{s})$	\rightarrow	$\text{Ni}(\text{s})$	+	$\text{CH}_4(\text{s})$
R29	$\text{Ni}(\text{s})$	+	$\text{CH}_3(\text{s})$	\rightarrow	$\text{H}(\text{s})$	+	$\text{CH}_2(\text{s})$
R30	$\text{H}(\text{s})$	+	$\text{CH}_2(\text{s})$	\rightarrow	$\text{Ni}(\text{s})$	+	$\text{CH}_3(\text{s})$
R31	$\text{Ni}(\text{s})$	+	$\text{CH}_2(\text{s})$	\rightarrow	$\text{H}(\text{s})$	+	$\text{CH}(\text{s})$
R32	$\text{H}(\text{s})$	+	$\text{CH}(\text{s})$	\rightarrow	$\text{Ni}(\text{s})$	+	$\text{CH}_2(\text{s})$
R33	$\text{Ni}(\text{s})$	+	$\text{CH}(\text{s})$	\rightarrow	$\text{H}(\text{s})$	+	$\text{C}(\text{s})$
R34	$\text{H}(\text{s})$	+	$\text{C}(\text{s})$	\rightarrow	$\text{Ni}(\text{s})$	+	$\text{CH}(\text{s})$
Surface Reactions (involving C, O and H)							
R35	$\text{CH}_4(\text{s})$	+	$\text{O}(\text{s})$	\rightarrow	$\text{OH}(\text{s})$	+	$\text{CH}_3(\text{s})$
R36	$\text{OH}(\text{s})$	+	$\text{CH}_3(\text{s})$	\rightarrow	$\text{CH}_4(\text{s})$	+	$\text{O}(\text{s})$
R37	$\text{CH}_3(\text{s})$	+	$\text{O}(\text{s})$	\rightarrow	$\text{OH}(\text{s})$	+	$\text{CH}_2(\text{s})$
R38	$\text{OH}(\text{s})$	+	$\text{CH}_2(\text{s})$	\rightarrow	$\text{CH}_3(\text{s})$	+	$\text{O}(\text{s})$
R39	$\text{CH}_2(\text{s})$	+	$\text{O}(\text{s})$	\rightarrow	$\text{OH}(\text{s})$	+	$\text{CH}(\text{s})$
R40	$\text{OH}(\text{s})$	+	$\text{CH}(\text{s})$	\rightarrow	$\text{CH}_2(\text{s})$	+	$\text{O}(\text{s})$
R41	$\text{CH}(\text{s})$	+	$\text{O}(\text{s})$	\rightarrow	$\text{OH}(\text{s})$	+	$\text{C}(\text{s})$
R42	$\text{OH}(\text{s})$	+	$\text{C}(\text{s})$	\rightarrow	$\text{CH}(\text{s})$	+	$\text{O}(\text{s})$

Deutschmann, O., Tischer, S., Schaedel, B., and Maier, L., Surface reactions: reforming and oxidation of methane on nickel, <http://www.detchem.com/mechanisms/nickel.html>, (01/03/06)

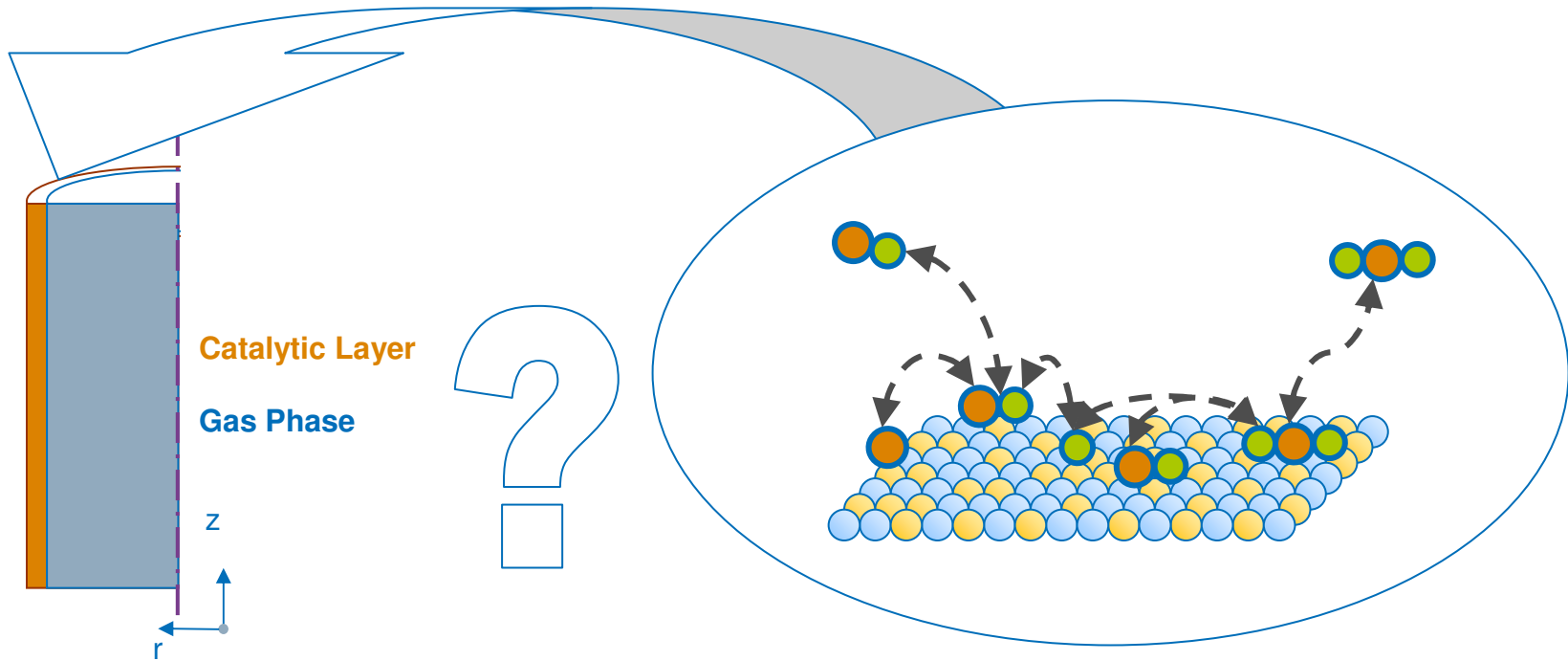
Problem Definition: Chemical Reaction Mechanism



Surface Adsorption/Desorption Reactions					
R1	H ₂	+	2Ni(s)	→	2H(s) + 2Ni(s)
R2			2H(s)	→	H ₂ + 2Ni(s)
R3	O ₂	+	2Ni(s)	→	2O(s) + 2Ni(s)
R4			2O(s)	→	O ₂ + 2Ni(s)
R5	CH ₄	+	Ni(s)	→	CH ₄ (s) + Ni(s)
R6			CH ₄ (s)	→	CH ₄ + Ni(s)
R7	H ₂ O	+	Ni(s)	→	H ₂ O(s) + Ni(s)
R8			H ₂ O(s)	→	H ₂ O + Ni(s)
R9	CO ₂	+	Ni(s)	→	CO ₂ (s) + Ni(s)
R10			CO ₂ (s)	→	CO ₂ + Ni(s)
R11	CO	+	Ni(s)	→	CO(s) + Ni(s)
R12			CO(s)	→	CO + Ni(s)
Surface Reactions (involving O, H and Ni atoms)					
R13	H(s)	+	O(s)	→	Ni(s) + OH(s)
R14	Ni(s)	+	OH(s)	→	H(s) + O(s)
R15	H(s)	+	OH(s)	→	Ni(s) + H ₂ O(s)
R16	Ni(s)	+	H ₂ O(s)	→	H(s) + OH(s)
R17			2OH(s)	→	H ₂ O(s) + O(s)
R18	H ₂ O(s)	+	O(s)	→	2OH(s)
Surface Reactions (involving O, C and Ni atoms)					
R19	C(s)	+	O(s)	→	Ni(s) + CO(s)
R20	Ni(s)	+	CO(s)	→	C(s) + O(s)
R21	CO(s)	+	O(s)	→	Ni(s) + CO ₂ (s)
R22	Ni(s)	+	CO ₂ (s)	→	CO(s) + O(s)
Surface Reactions (involving C, O, H and Ni atoms)					
R23	Ni(s)	+	HCO(s)	→	H(s) + CO(s)
R24	H(s)	+	CO(s)	→	Ni(s) + HCO(s)
R25	Ni(s)	+	HCO(s)	→	CH(s) + O(s)
R26	CH(s)	+	O(s)	→	Ni(s) + HCO(s)
Surface Reactions (involving C, H and Ni atoms)					
R27	Ni(s)	+	CH ₄ (s)	→	H(s) + CH ₃ (s)
R28	H(s)	+	CH ₃ (s)	→	Ni(s) + CH ₄ (s)
R29	Ni(s)	+	CH ₃ (s)	→	H(s) + CH ₂ (s)
R30	H(s)	+	CH ₂ (s)	→	Ni(s) + CH ₃ (s)
R31	Ni(s)	+	CH ₂ (s)	→	H(s) + CH(s)
R32	H(s)	+	CH(s)	→	Ni(s) + CH ₂ (s)
R33	Ni(s)	+	CH(s)	→	H(s) + C(s)
R34	H(s)	+	C(s)	→	Ni(s) + CH(s)
Surface Reactions (involving C, O and H)					
R35	CH ₄ (s)	+	O(s)	→	OH(s) + CH ₃ (s)
R36	OH(s)	+	CH ₃ (s)	→	CH ₄ (s) + O(s)
R37	CH ₃ (s)	+	O(s)	→	OH(s) + CH ₂ (s)
R38	OH(s)	+	CH ₂ (s)	→	CH ₃ (s) + O(s)
R39	CH ₂ (s)	+	O(s)	→	OH(s) + CH(s)
R40	OH(s)	+	CH(s)	→	CH ₂ (s) + O(s)
R41	CH(s)	+	O(s)	→	OH(s) + C(s)
R42	OH(s)	+	C(s)	→	CH(s) + O(s)

Deutschmann, O., Tischer, S., Schaedel, B., and Maier, L., Surface reactions: reforming and oxidation of methane on nickel, <http://www.detchem.com/mechanisms/nickel.html>, (01/03/06)

Problem Definition:



Cylindrical Channel

How the surface reaction mechanism can be integrated in this geometry using COMSOL?

Catalytic Layer Modeling

Two different approaches

Catalytic Thin Volume (VM)

Easy to model in COMSOL, by using 2 domains

By **conserving** the total **catalytic sites** and the **total Volume**

$$Ni_{total} \left(\frac{mol}{m^2} \right) \frac{Surf \left(\frac{m^2}{m^3} \right)}{Vol \left(\frac{m^3}{m^3} \right)}$$

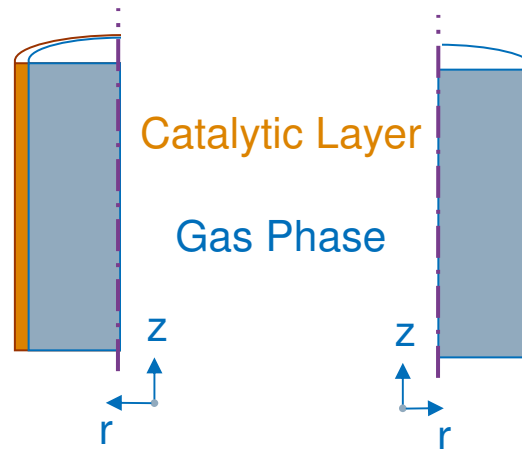
Conversion of the chemical reaction model from **surface to volume**

Catalytic Surface (SM)

Coupling of 1D/2D domains by, for example: **Boundary weak form**

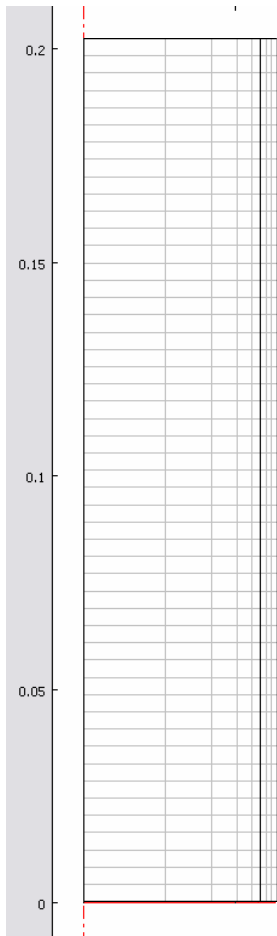
$$\frac{\partial C_{s_k}}{\partial t} = R, \quad \begin{matrix} \curvearrowright \\ \text{dweak} = c_test * c_time \\ \text{weak} = c_test * R \end{matrix}$$

Direct use of the surface **chemical reaction model**

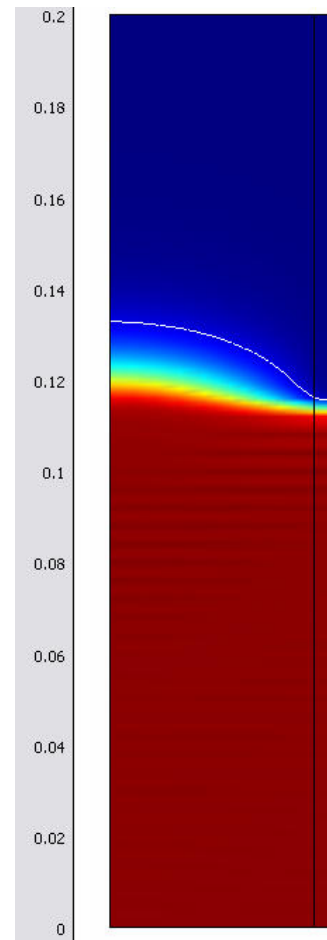


CONCLUSION:
Both cases are simulated

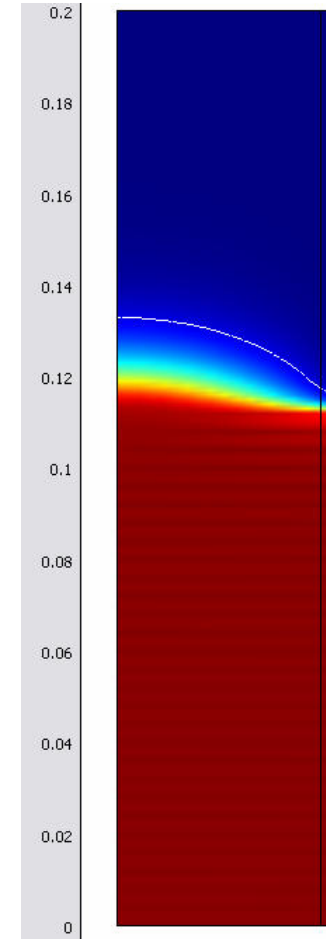
Catalytic Layer Modeling: for surface O₂ adsorption



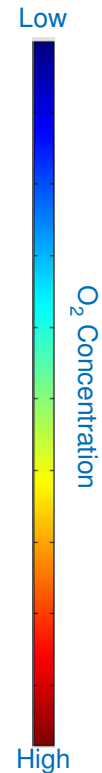
Run Simulation:
• In transient mode
• Up to 1s



VM Case



SM Case



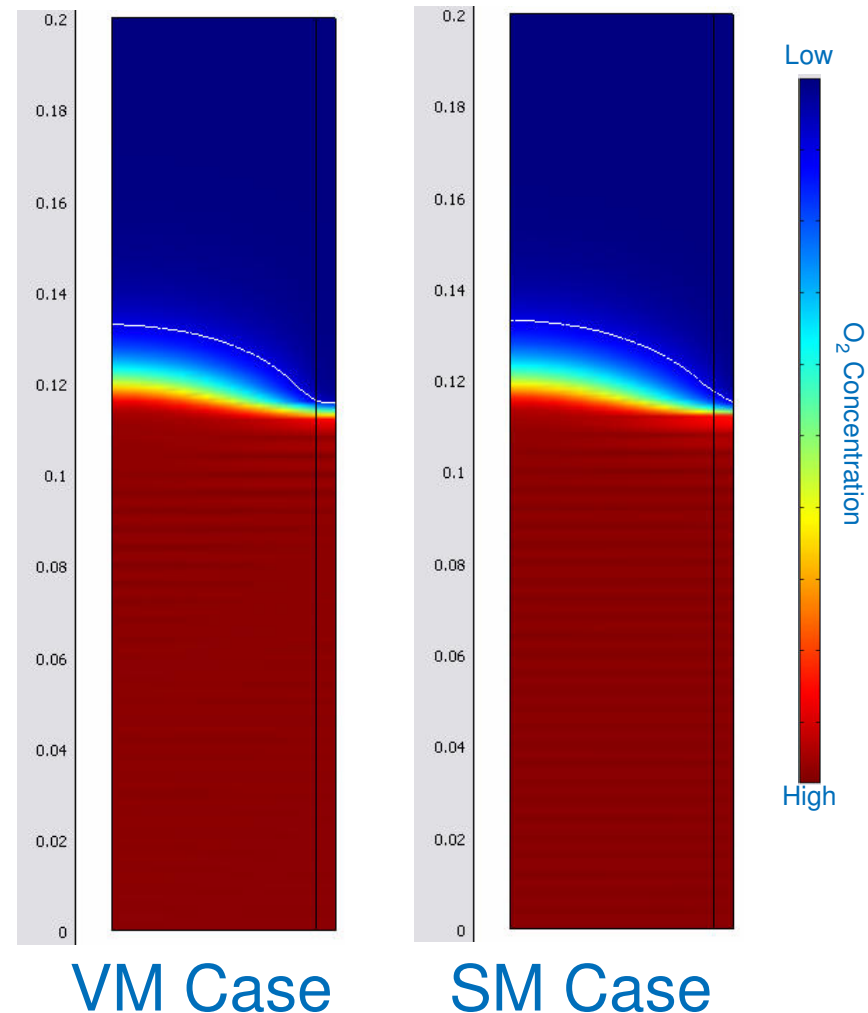
© IFP Draw and Mesh

Catalytic Layer Modeling: for surface O₂ adsorption

- The results are similar, then:
 - The two approaches are equivalent
 - The chemical mechanism conversion from surface to volume is reasonable
- The SM is better than VM in terms of calculation time

	COMSOL 3.4
VM	1016
SM	533
Model Comparison	-48%

$$\frac{t_{SM} - t_{VM}}{t_{VM}}$$



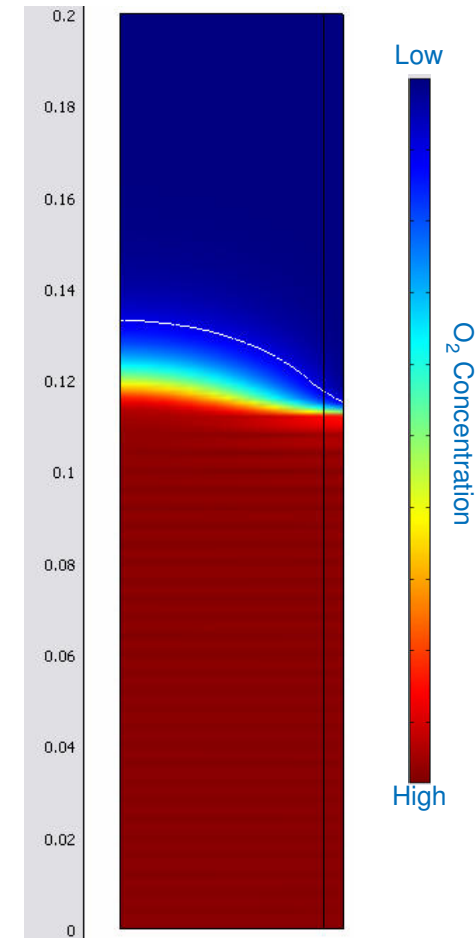
Catalytic Layer Modeling: for surface O₂ adsorption

- The results are similar, then:
 - The two approaches are equivalent
 - The chemical mechanism conversion from surface to volume is reasonable
- The SM is better than VM in terms of calculation time

	COMSOL 3.4	COMSOL 3.5	Version Comparison
VM	1016	337	- 67%
SM	533	126	- 76%
Model Comparison	- 48%	- 63%	

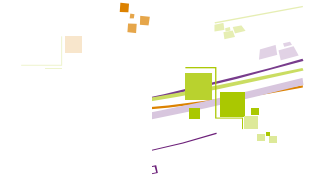
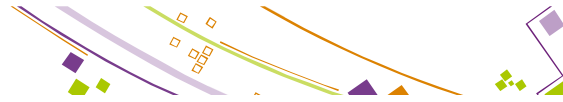
$$\frac{t_{3.5} - t_{3.4}}{t_{3.4}}$$

Fails with 42 surface reactions





SM Case

$$\frac{t_{SM} - t_{VM}}{t_{VM}}$$



Main Objectives

- The Objective is to build an isothermal reactor model.
 - The problem geometry is defined by: 
 - Axial symmetric geometry
 - Modeling the catalytic layer as surface using boundary weak form
 - The governing equations are defined by: 
 - Hydrodynamic: Poiseuille
 - Mass balance equations
 - Surface chemical reactions
- We will:
 - Show you the main simulation
 - Evaluate the simulator trends

ATR Monolithic Reactor Modeling:

- 7 gas species

- H₂, O₂, H₂O, CH₄, CO, CO₂ and N₂

$$\Rightarrow 7x \frac{\partial C_k}{\partial t} + \nabla \cdot (-D \nabla C_k + C_k u) = R$$

Convection and Diffusion
Chemical Engineering Module

- 13 adsorbed species

- H₂O_s, OH_s, H_s, O_s, C_s, CO_s, CO_{2s}, CH_{4s}, CH_{3s}, CH_{2s}, CH_s, HCO_s and Ni

$$\Rightarrow \begin{array}{l} 12x \frac{\partial C_{s_k}}{\partial t} = R \\ 1x \text{ site balance} \end{array}$$

$$\begin{array}{l} \text{dweak} = c_test * c_time \\ \text{weak} = c_test * R \end{array}$$

Boundary Weak Form
PDE Modes

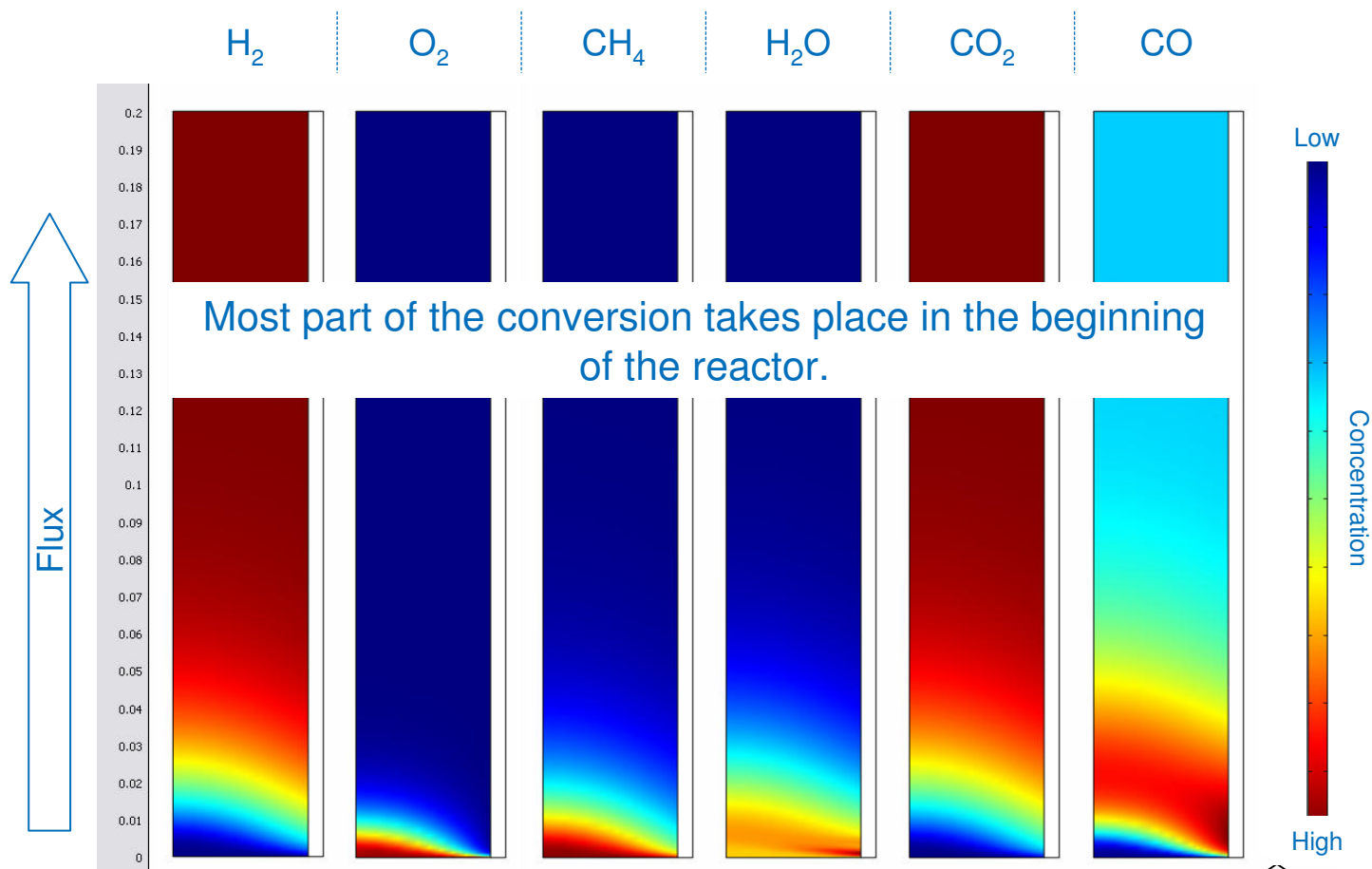
20 equations

- 42 surface chemical reactions

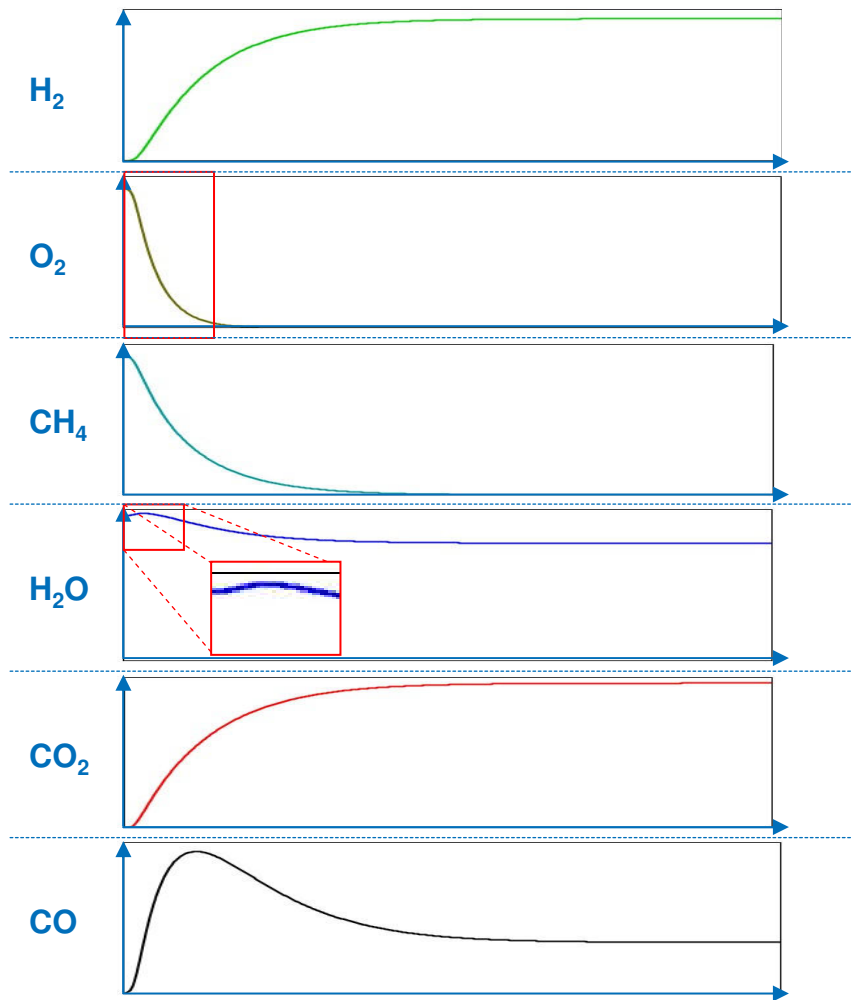
- Time-dependent solver until the steady state, being the initial values for:

- All gas species = injection concentration
 - to avoid the concentration front wave calculation
 - Ni = total catalytic site density then all other solid species = 0

ATR Monolithic Reactor Modeling: Simulation Concentration Profiles

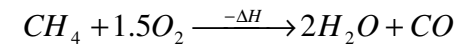


ATR monolithic reactor modeling: Concentration profiles in channel axis



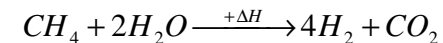
■ First observation: Partial Oxidation

- The O₂ is totally converted and fast
- An amount of H₂O and CO is formed



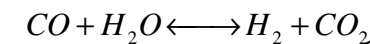
■ Second observation: Steam Reforming

- The H₂O is consumed
- The CH₄ is almost totally converted
- CO₂ and H₂ are produced

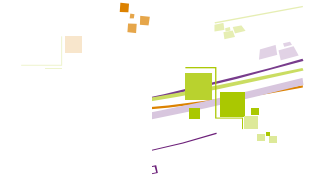
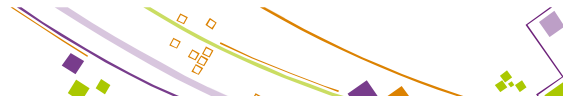


■ Third observation: Water Gas Shift





- CO and H₂O are converted into H₂ and CO₂ till the equilibrium state



The result trends are as expected



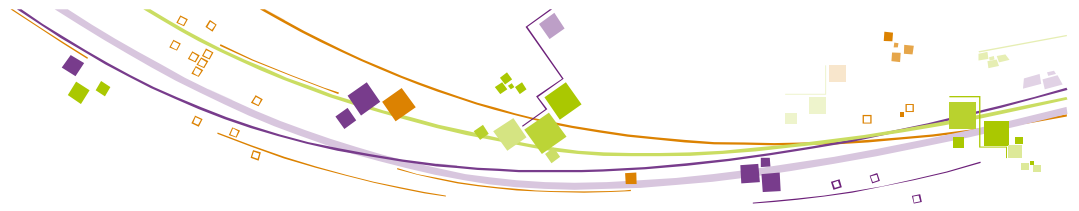
Main Objectives

- **The Objective is to build an isothermal reactor model.**
 - **The problem geometry is defined by:** 
 - Axial symmetric geometry
 - Modeling the catalytic layer as surface using boundary weak form
 - **The governing equations are defined by:** 
 - Hydrodynamic: Poiseuille
 - Mass balance equations
 - Surface chemical reactions
 - **The main simulation was run:** 
 - For 7 gas species and 13 adsorbed species
 - Resulting in 20 mass balance equations
 - Interlinked by 42 surface chemical reactions
 - **The simulator trends was evaluated by the presence of :** 
 - Partial oxidation
 - Steam reforming to produce H₂
 - Water gas shift equilibrium



Conclusions

- To model a catalytic surface we suggest using the Boundary Weak Form application
- A simulator of an ATR monolithic reactor is now ready to use and to be improved, namely:
 - by adding hydrodynamic and thermal effects



Acknowledgements

- The authors thank :
 - ANRT for the financial support
 - COMSOL team for help

...and you for your attention