

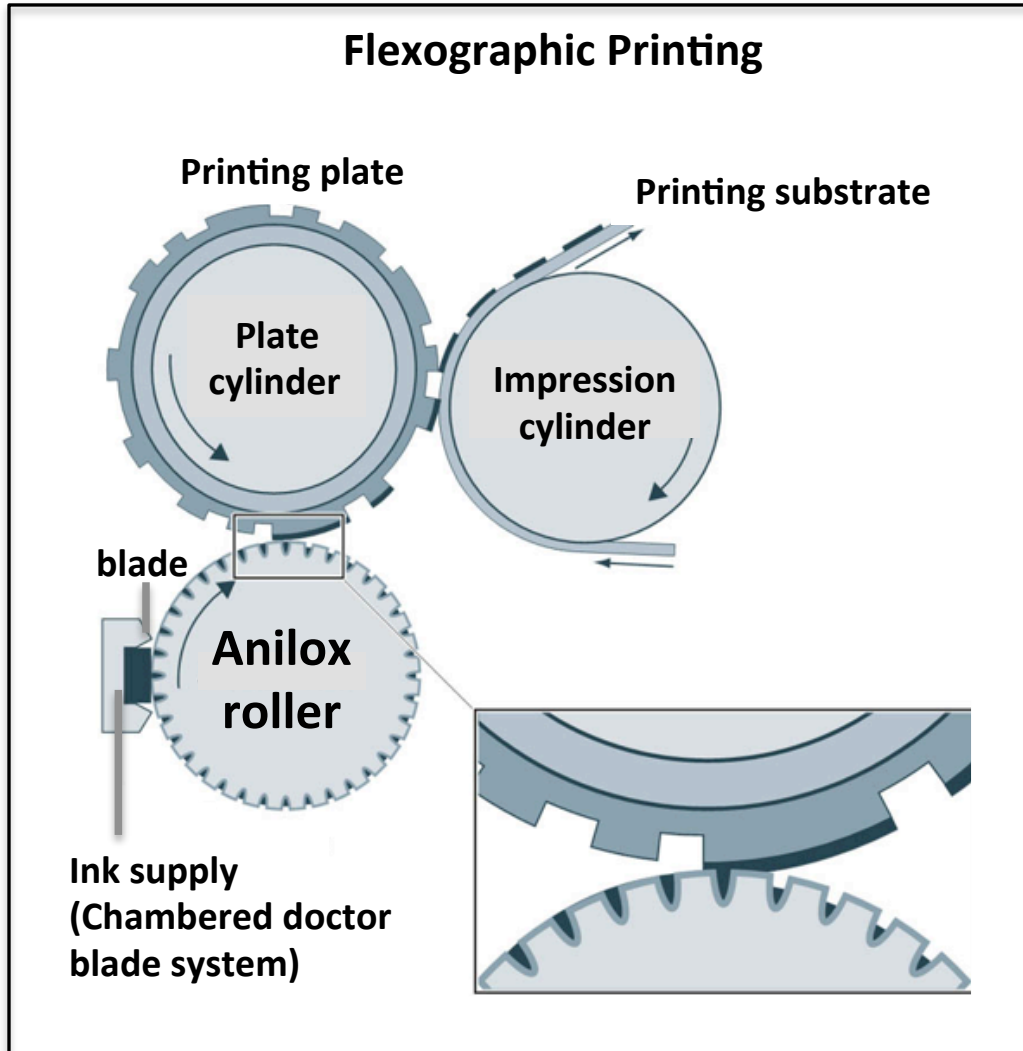
Effect of Substrate Contact Angle on Ink Transfer in Flexographic Printing

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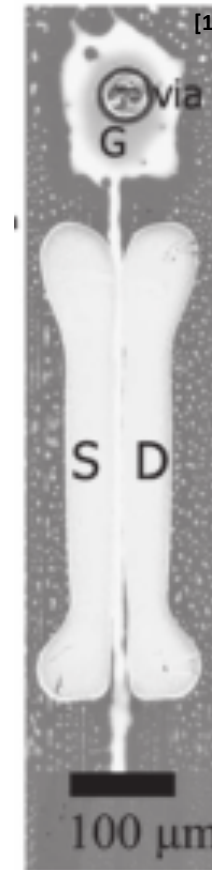
Outline

- Introduction
- Motivation and Objectives
- Simulations
- . Methodology
- . Results
- Conclusions and Future Work

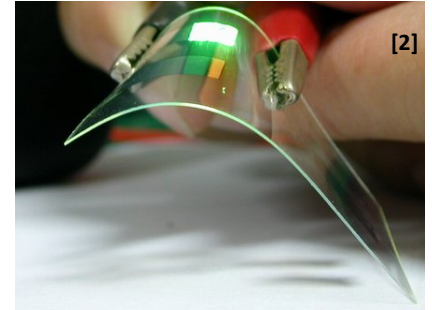
Flexography



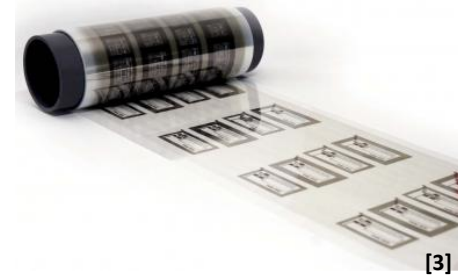
thin film transistor



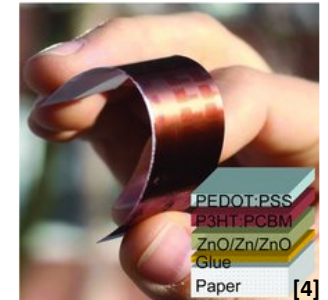
OLED



RFID

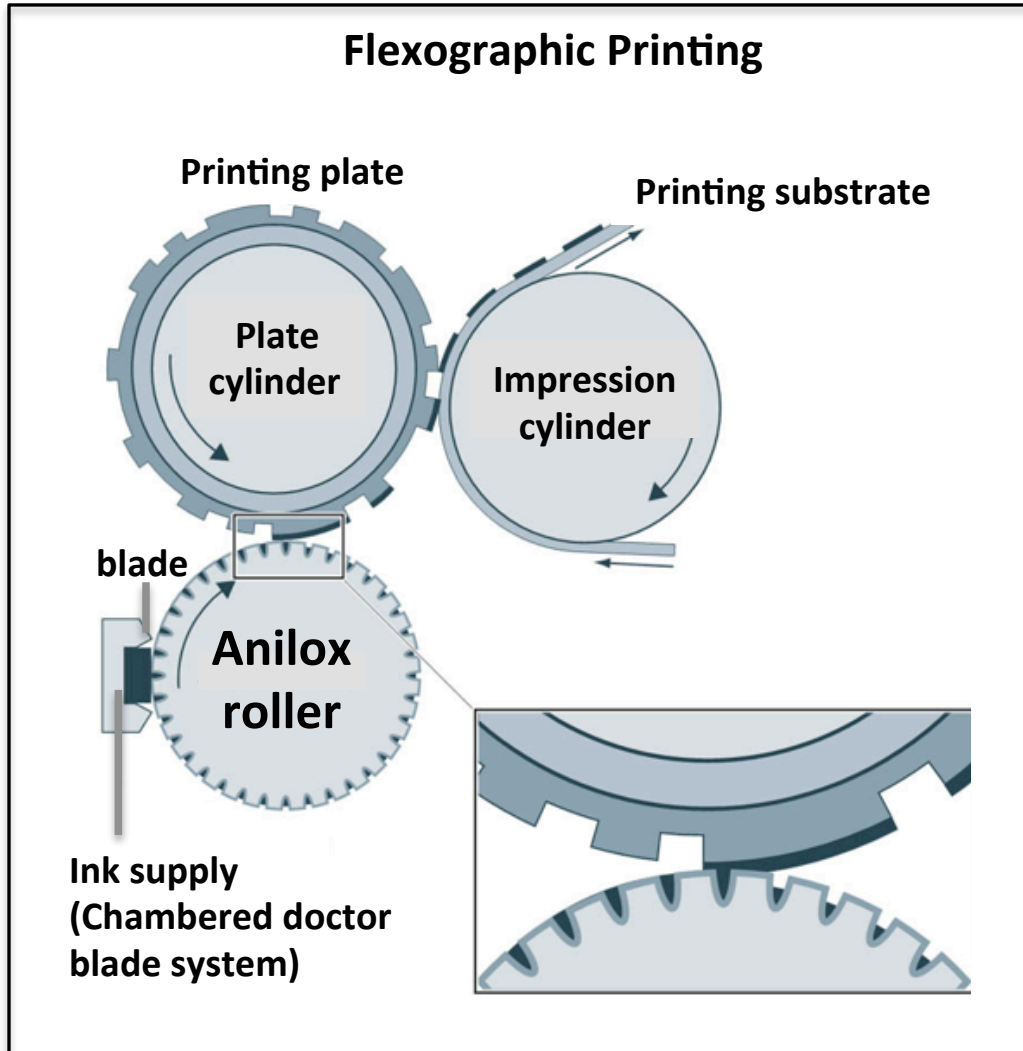


photovoltaic cell



- [1] H. Kang *et al.*, *Advanced Materials*, 2012
- [2] Wikimedia/meharris
- [3] Gyou-Jin Cho/Sunchon National University
- [4] A. Hubler *et al.*, *Advanced Energy Materials*, 2011

Ink Transfer in Flexography



INK TRANSFER TO THE ANILOX ROLLER



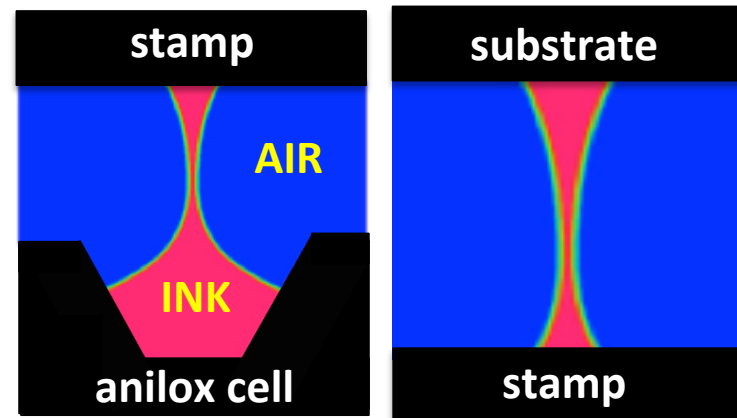
BLADING OF THE ANILOX ROLLER
(fill the cells + remove excess ink layer)



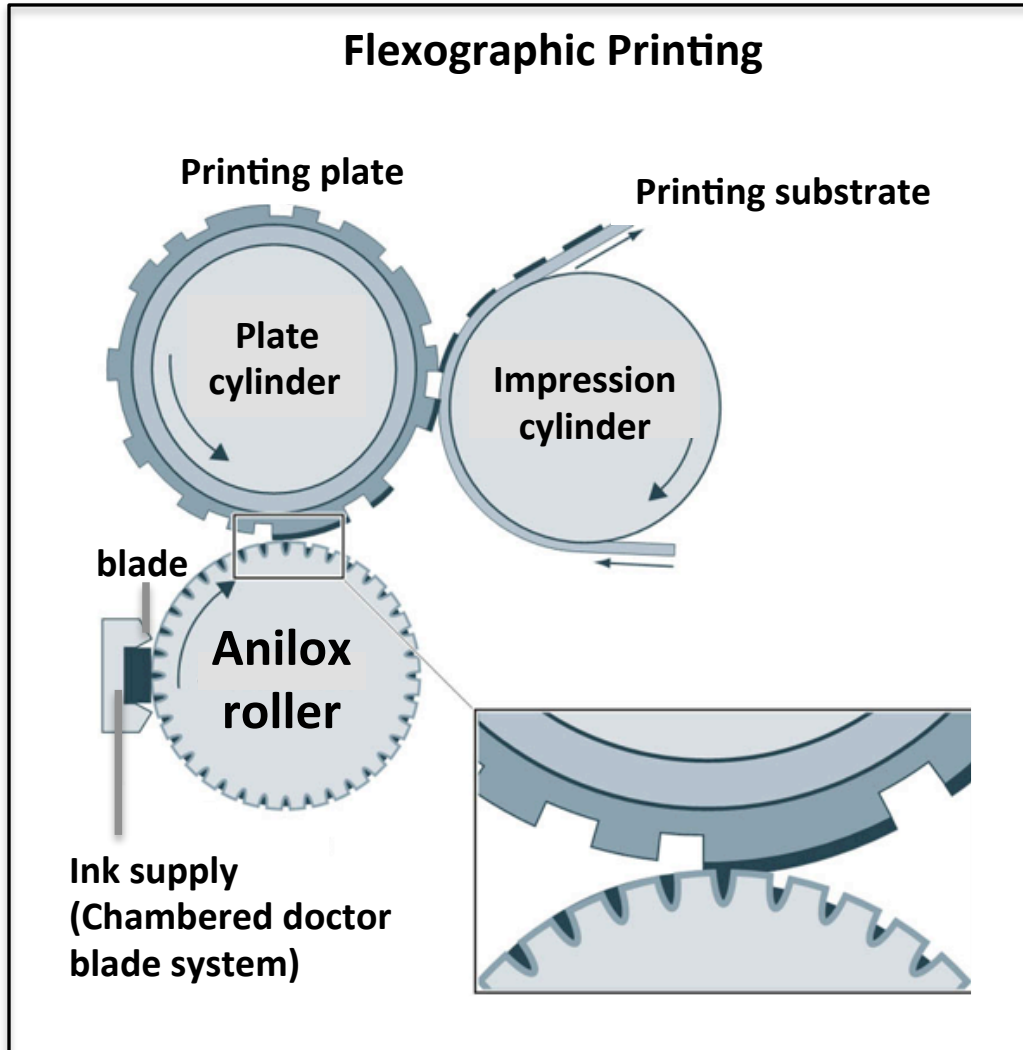
INKING OF THE STAMP
(partial cell evacuation by ink splitting)



INK TRANSFER TO THE SUBSTRATE
(ink splitting)



Ink Transfer in Flexography

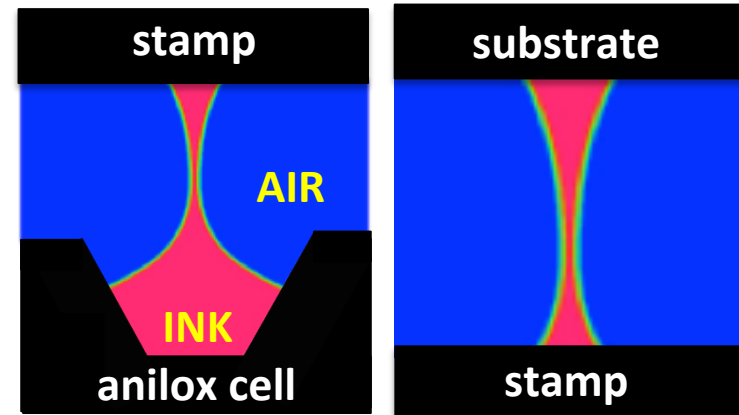


INK TRANSFER TO THE ANILOX ROLLER

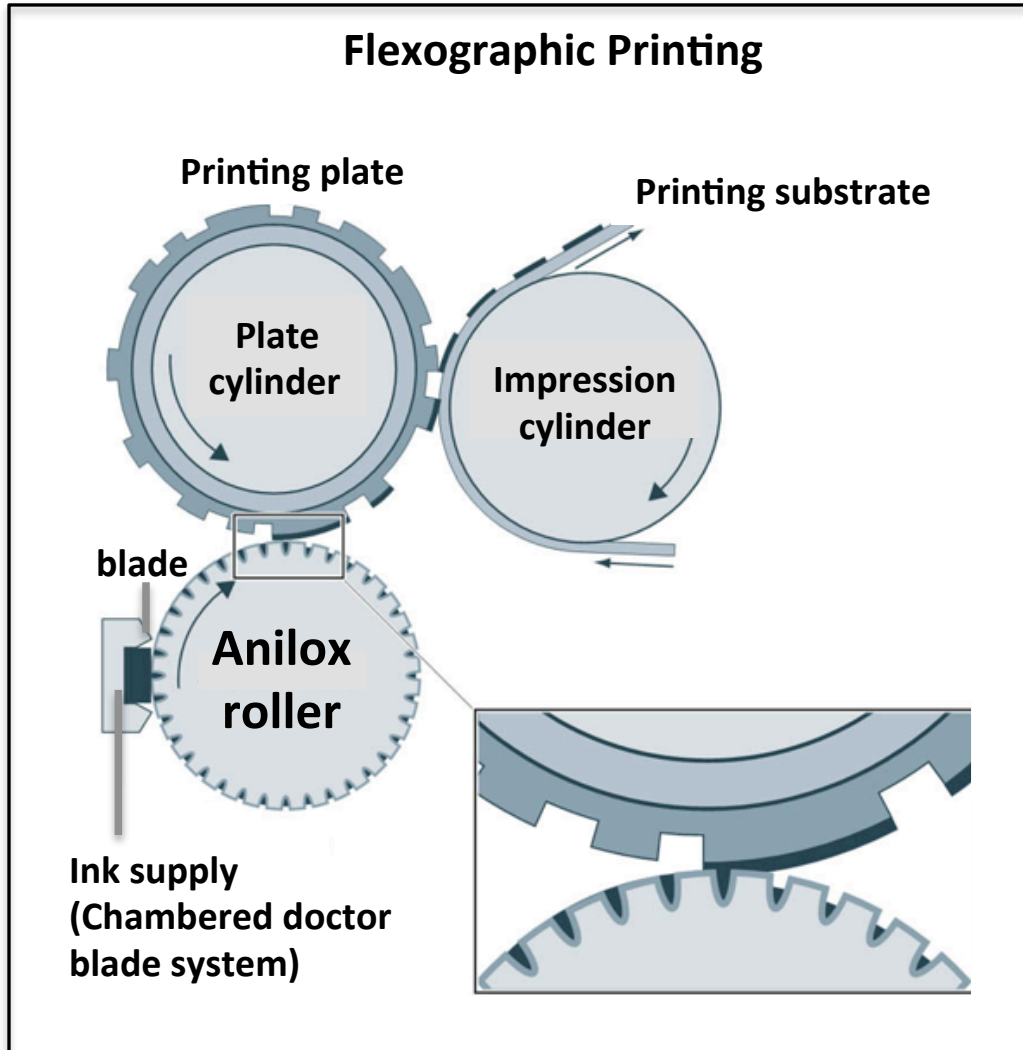
BLADING OF THE ANILOX ROLLER
(fill the cells + remove excess ink layer)

INKING OF THE STAMP
(partial cell evacuation by ink splitting)

INK TRANSFER TO THE SUBSTRATE
(ink splitting)



Motivation and Objectives

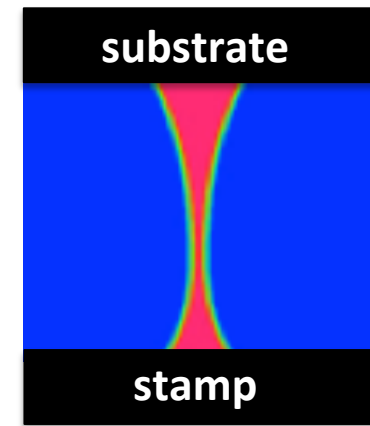


Ink Transfer from Stamp to Substrate

- Thickness of printed product
- Device performance

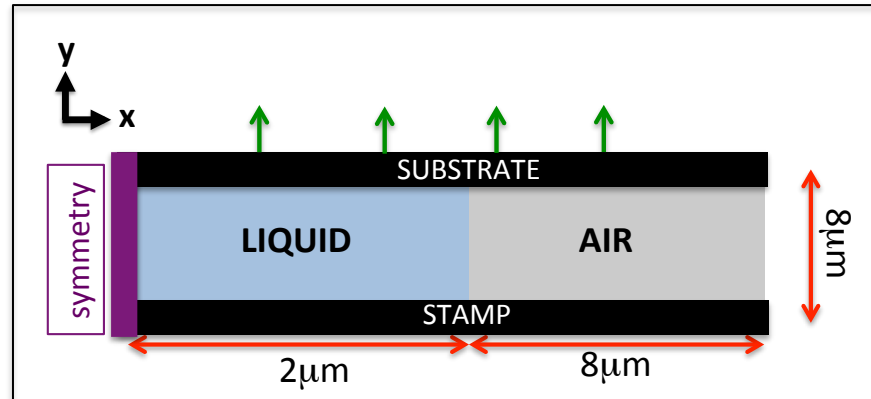
Objectives

- Guidelines for substrate and stamp design
- Control printed layer thickness
- Investigate contact angle effects



Simulation Domain

Simulation domain and its dimensions

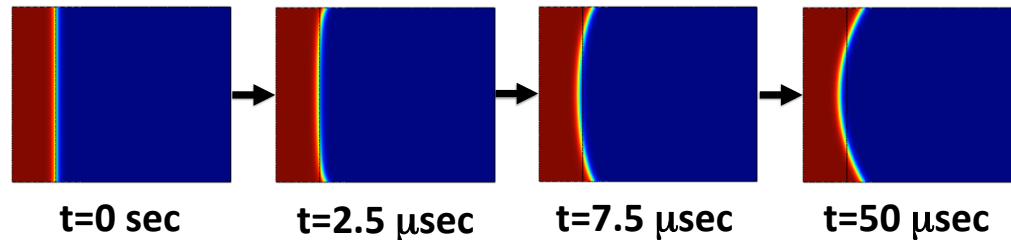


Parameters used in the simulation

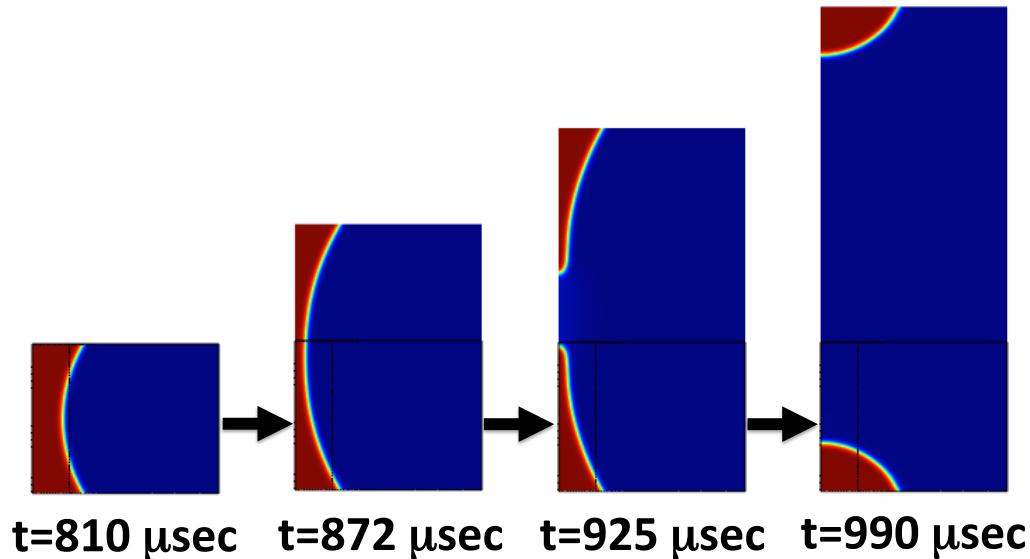
Ink dynamic viscosity	$0.1 \text{ N}\cdot\text{s}/\text{m}^2$
Ink density	$1000 \text{ kg}/\text{m}^3$
Air dynamic viscosity	$1.81\text{e-}5 \text{ N}\cdot\text{s}/\text{m}^2$
Air density	$1.16 \text{ kg}/\text{m}^3$
Gravity acceleration	0
Separation speed	0.1 m/s
Volume of liquid	$32\mu\text{m}^2$
Surface tension coefficient	1 N/m

Simulation Setup

Interface Reaches Equilibrium Shape

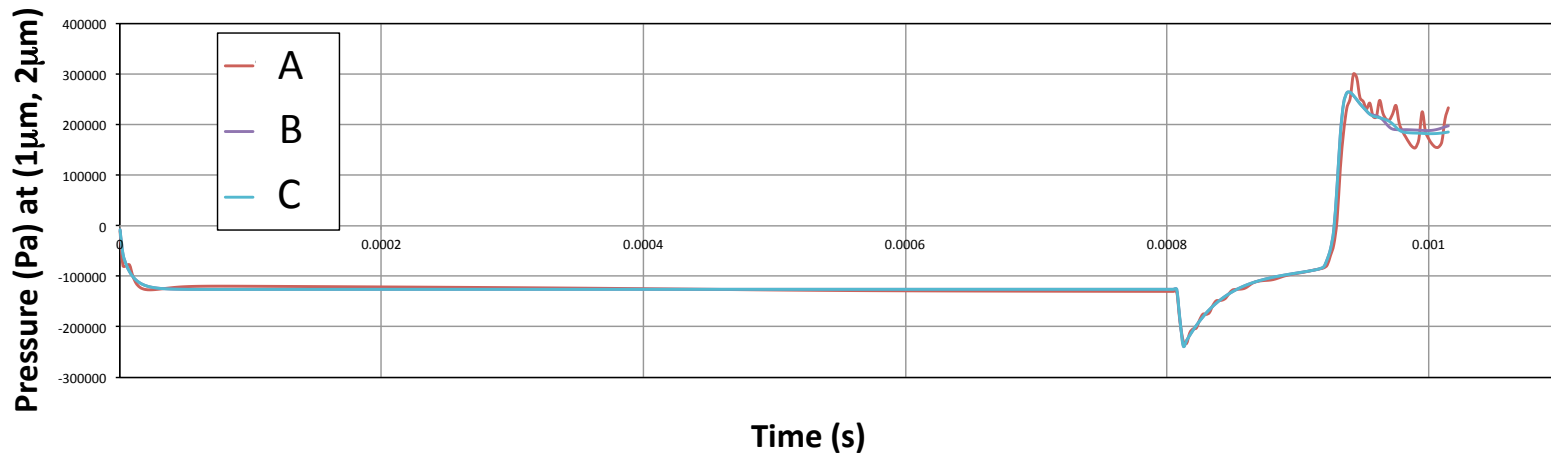
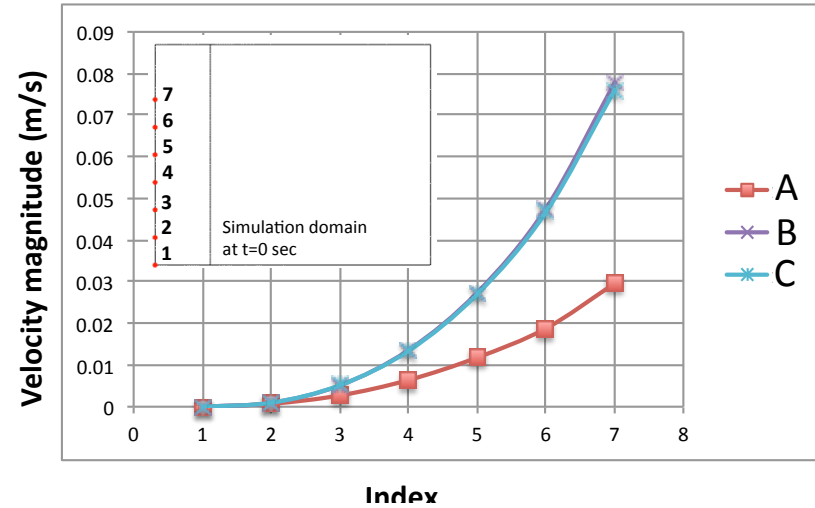
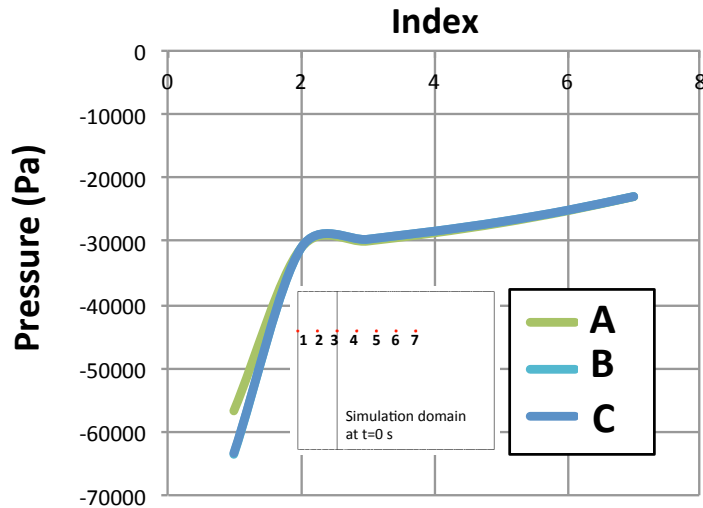


Ink splits into Two



- **Moving mesh interface** is coupled with **laminar two-phase flow, phase field interface**.
- Initial velocity and pressure values are set to zero for the two fluids.
- Initial mesh displacement is set to zero.
- Pressure is set to zero at right boundary which is defined as inlet.
- Stationary bottom surface is defined as “wetted wall” with 60° ink contact angle.
- Upper surface is defined as “moving wetted wall” with 60° contact angle.

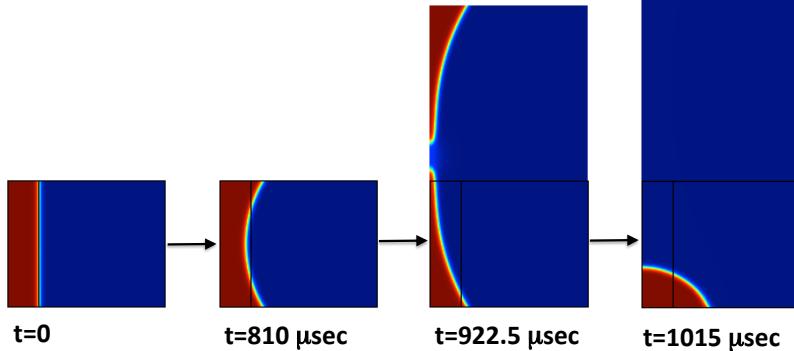
Mesh Refinement ($\theta_{\text{top}} = \theta_{\text{bottom}} = 60^\circ$)



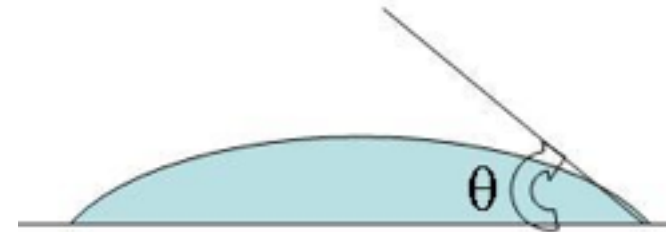
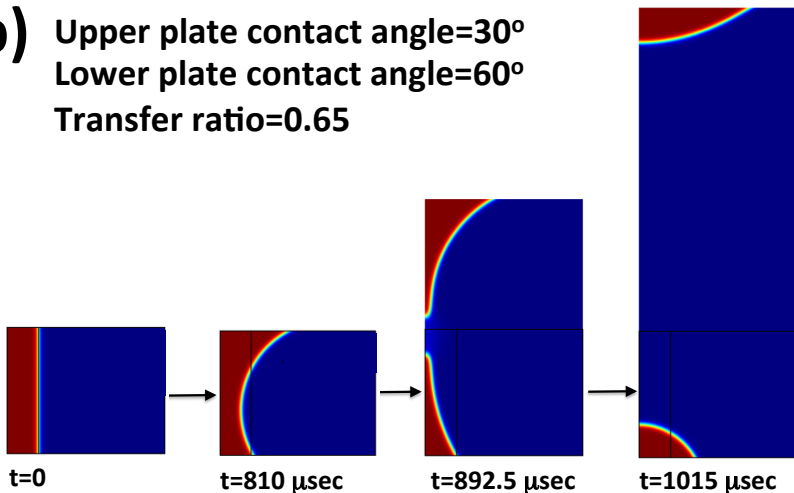
Maximum mesh element size for left of domain: A → 0.25 μm, B → 0.08 μm, C → 0.06 μm
 Change in total mass < 2%

Effect of Contact Angle

a) Upper plate contact angle=60°
Lower plate contact angle=60°
Transfer ratio=0.5



b) Upper plate contact angle=30°
Lower plate contact angle=60°
Transfer ratio=0.65



Young-Dupre Equation

$$W_{\text{adhesion}} = \gamma \cdot [1 + \cos(\theta)] \rightarrow \theta \downarrow W_{\text{adhesion}} \uparrow$$

Results

- Expected trend is observed
- Results do not exactly match with literature
- High computation times

Conclusions and Future Work

- Splitting of ink between two parallel plates is simulated
- Ink transfer ratio to the upper plate is found to increase with decreasing ink contact angle on its surface
- High computation times due to fine mesh requirements is the main difficulty
- Future work is to cover a larger range of contact angles in the simulations

Thank you

Q&A