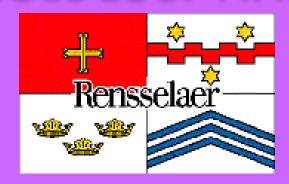
MODELING ACOUSTIC MODES IN A CONTINUOUS LOOP PIPING SYSTEM



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Background

- Closed loop piping systems are a series of inter-connected cylindrical shells intended to transport a fluid from one location to another and are widely used in industry.
- In these systems, the fluid passes from a starting point along a supply path to a location where the quantity within the fluid is transferred into another process through a component such as a heat exchanger, separator or hydraulic actuator. Once the quantity of interest has been transferred, the fluid is recirculated through a return leg to the original location forming a "continuous" loop of fluid.
- Two common examples are hydraulic and heating/coolant systems.

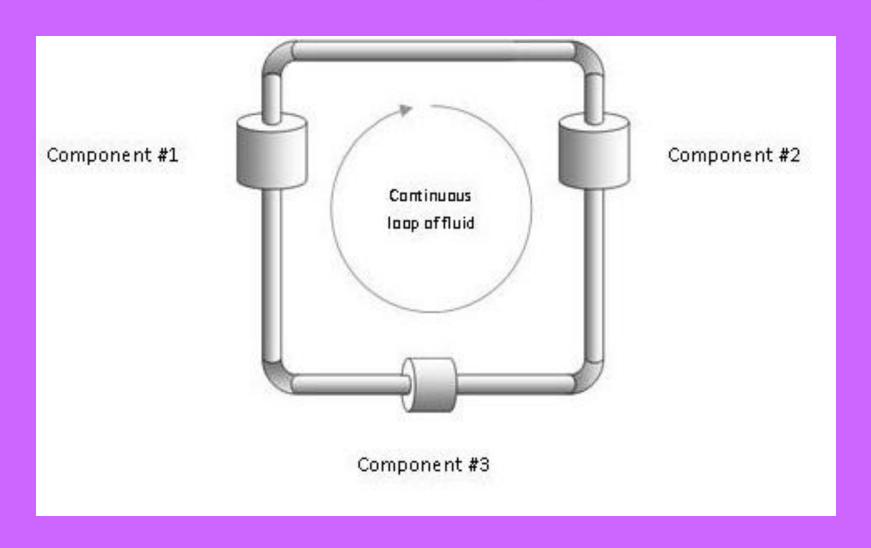


Motivation and Objective

- Fluid resonances can detrimentally impact the operation of fluid systems and components. The unwanted impacts of the fluid resonances include increased system noise, excessive component fatigue, interference with test measurements and monitoring instrumentation, improper system and potentially system or component failure.
- The purpose of the study was to accurately determine the frequency and mode shapes of low frequency axial fluid resonances within a system of piping and components that form a continuous loop.



Schematic of a Simple Closed Loop Piping System





Assumptions/Limitations

- Closed system; Free-free boundary condition
- Neglect body forces and the effects of pipe or component foundations
- The structures of the piping and component walls are assumed to be either rigid or linearly elastic (steel)
- The internal fluid (water) is a liquid and assumed to be free from bubbles or dissolved particulates. The fluid will also be assumed to be at rest and at a uniform temperature and pressure
- The axial loop resonances investigated are restricted to resonances of the lowest order axially symmetric radial mode or plane waves



Material and Piping Properties

Materials

| | Property . | Symbol | Metric | | English | |
|--------------|-----------------|----------------|----------|-------------------|-----------|--------------------|
| Material | | | Value | Units | Value | Units |
| Steel | Young's Modulus | E | 1.95E+11 | Pa | 2.8282E+7 | psi |
| | Shear Modulus | G | 8.30E+10 | Pa | 1.2038E+7 | psi |
| | Poisson's Ratio | ν | 0.28 | 7/ | 0.28 | ā |
| | Density | ρ | 7700 | kg/m ³ | 2.7818E-1 | lb/in ³ |
| | Speed of sound | Ca | 6100 | m/s | 2.4016E+5 | in/s |
| Aluminu m | Young's Modulus | Е | 7.1E+10 | Pa | 1.0298E+7 | psi |
| | Shear Modulus | G | 2.4E+10 | Pa | 3.4809E+6 | psi |
| | Poisson's Ratio | ν | 0.33 | 8 | 0.33 | - |
| | Density | ρ | 2700 | kg/m³ | 9.7543E-2 | lb/:n ³ |
| | Speed of sound | Cc | 6300 | m/s | 2.4803E+5 | in/s |
| Water* | Density | ρ | 998 | kg/m ³ | 3.6055E-2 | 1b/:n ³ |
| | Speed of Sound | c _o | 1481 | m/s | 58307.1 | in/s |
| | Bulk Modulus | Bf | 2.18E+9 | Pa | 3.1618E+5 | psi |

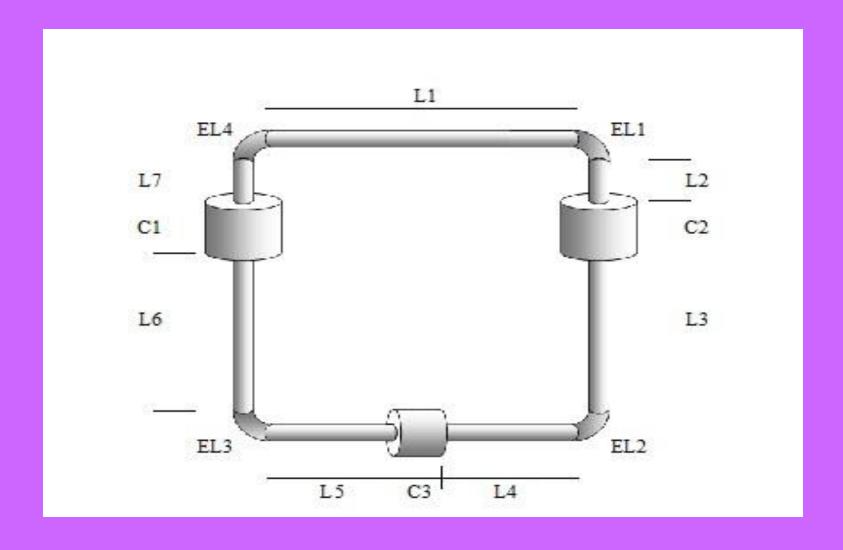
Piping

| Pipe | | Metric | units | English | units |
|-------------------|-----|----------|-------|---------|-------|
| Schedule | 8 | 80 | 12 | 80 | 2 |
| Nominal Pipe Size | NPS | 10 | - | 10 | - |
| Outer Diameter | OD | 27.305 | cm | 10.75 | in |
| Inner Diameter | ID | 24.29256 | cm | 9.564 | in |
| Thickness | h | 1.50622 | cm | 0.593 | in |
| Radius | a | 12.14628 | cm | 4.782 | in |

| Long Radius Elbow | Metric | units | English | units | |
|--------------------|-----------|----------|---------|----------------|-----|
| Outer Diameter | OD | 27.305 | cm | 10.75 | in |
| Inner Diameter | ID | 24.29256 | cm | 9.564 | in |
| Thickness | h | 1.50622 | cm | 0.593 | in |
| Bend Radius | R_{E} | 38.1 | cm | (1.5*NPS) = 15 | in |
| Bend Angle | β_E | π/2 | rad | 90 | deg |
| Center Line Length | Lca | 59.84723 | cm | 23.5619 | in |



Closed Loop Piping System Schematic





Closed Loop Piping System Details

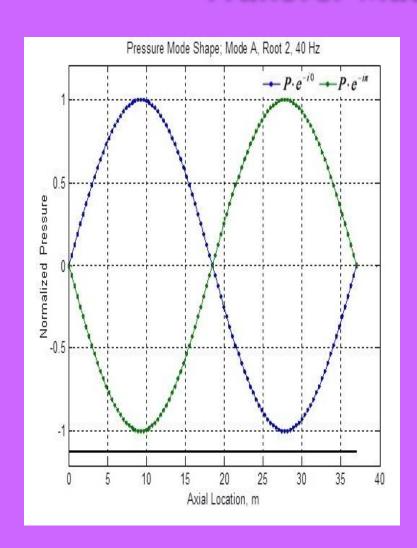
| Segment | # | Metric | Units | English | Units |
|-------------|-----------------|--------------------------------|----------|---------------------------------|----------------|
| Length 1 | L1 EL1 L2 | 865.7777 59.84723 166.44 | cm cm | 2199.075 23.5619 422.7576 | in in in |
| Elbow 1 | | | | | |
| Length 2 | | | | | |
| Component 2 | C2 | 100 | cm | 254 | in |
| Length 3 | L3 | 599.3377 | cm | 1522.318 | in |
| Elbow 2 | EL2 | 59.84723 | cm | 23.5619 | in |
| Length 4 | L4 | 416.8885 | cm | 599.3377 | in |
| Component 3 | C3 | 33.0 | cm | 0.8382 | in |
| Length 5 | L5 | 416.8885 | cm | 599.3377 | in |
| Elbow 3 | EL3 | 59.84723 | cm | 23.5619 | in |
| Length 6 | L6 | 599.3377 | cm | 1522.318 | in |
| Component 1 | C1 | 100 | cm | 254 | in |
| Length 7 | L7 | 166.44 | cm | 422.7576 | in |
| Elbow 4 | EL4 | 59.84723 | cm | 23.5619 | in |

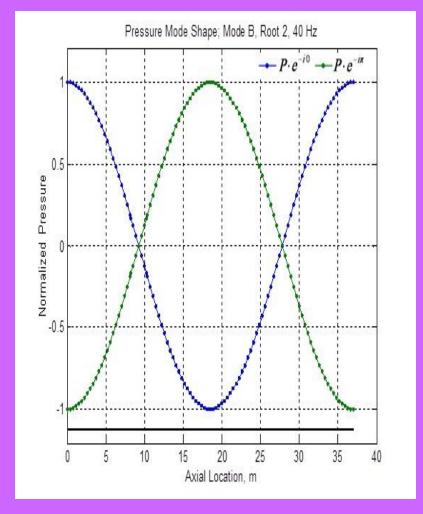


Governing Equation

$$\nabla^2 p - \left(\frac{1}{c_o^2}\right) \frac{\partial^2 p}{\partial t^2} = 0$$

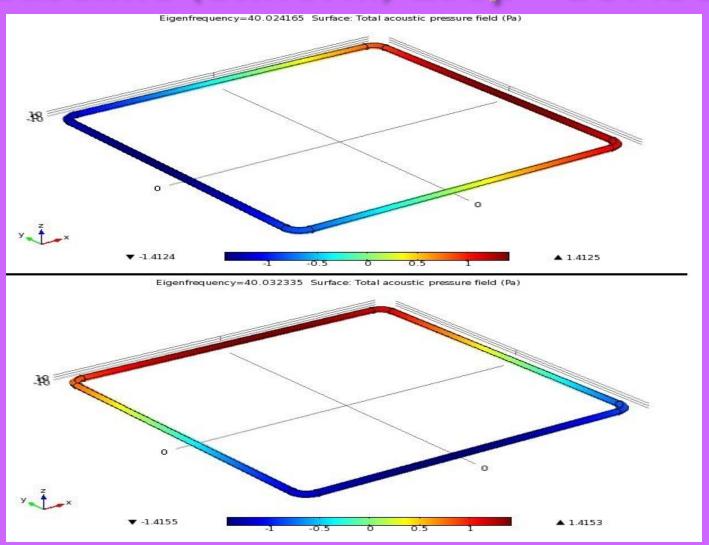
Results: Pressure Mode Shapes Baseline (uniform) Loop Transfer Matrix Method



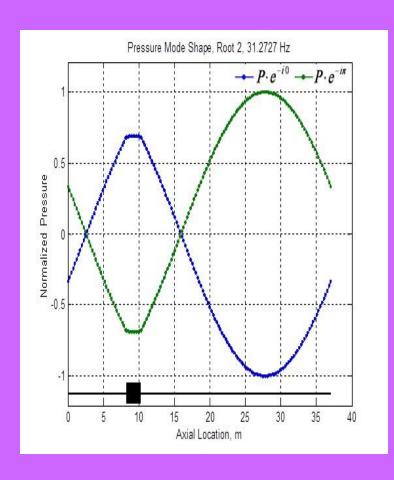


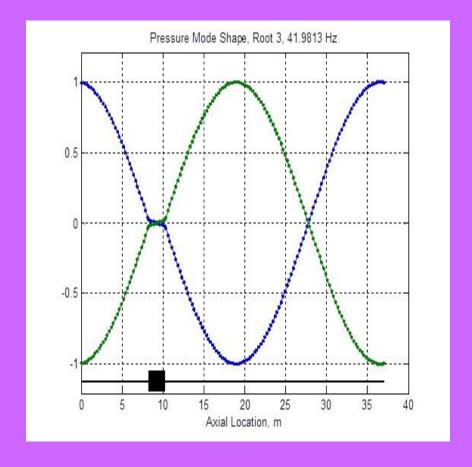


Pressure Mode Shapes Baseline (Uniform) Loop - COMSOL

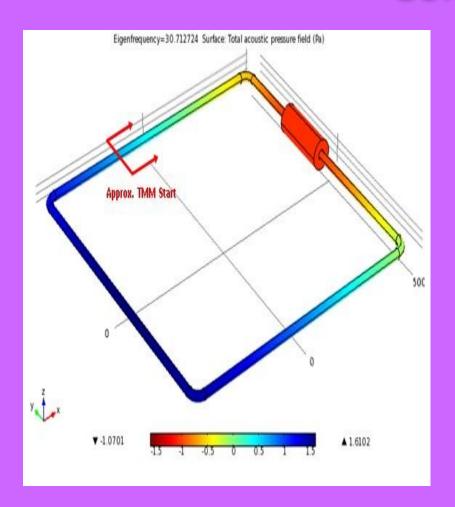


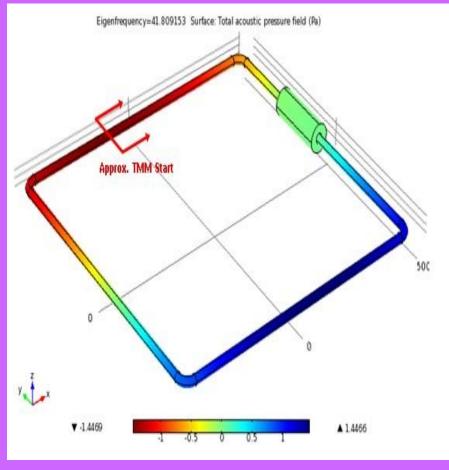
Results: Pressure Mode Shapes Loop with One Cavity Transfer Matrix Method



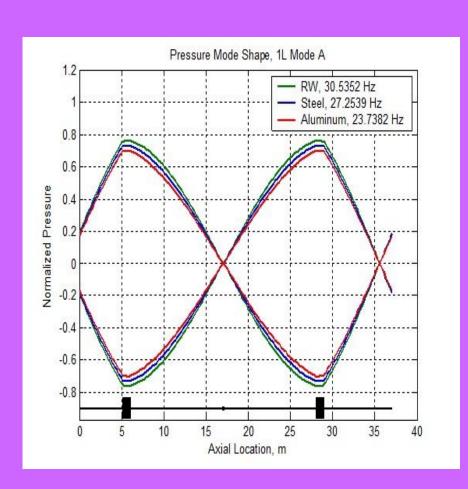


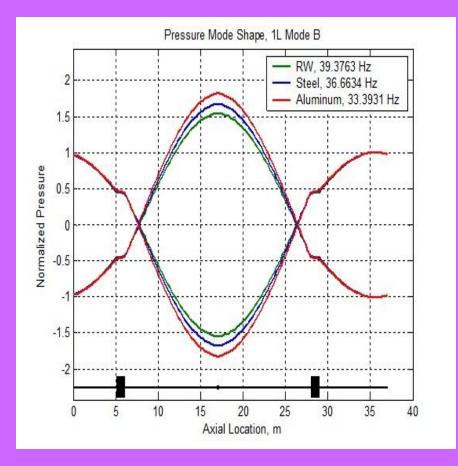
Results: Pressure Mode Shapes Loop with One Cavity COMSOL



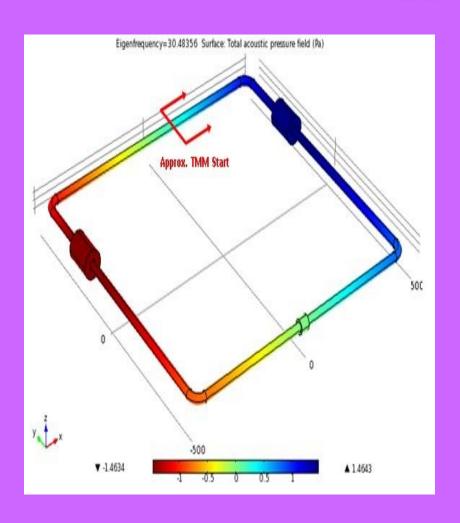


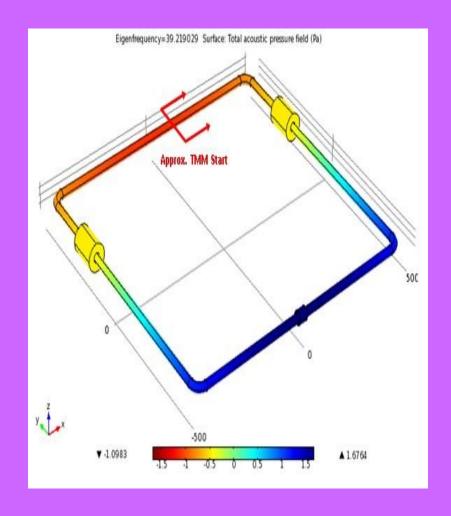
Results: Pressure Mode Shapes Loop with Three Cavities Transfer Matrix Method





Results: Pressure Mode Shapes Loop with Three Cavities COMSOL







Summary

- The pressure mode shapes were found to have a "kink" at the locations of the impedance and phase angle discontinuities.
- The changes in the frequency and mode shapes of the axial loop modes were much larger due to the impedance discontinuities than the changes in phase velocity due to the elasticity of the cylindrical components and piping.
- The frequencies and modes shapes of the axial loop modes calculated by the COMSOL FE models were in good agreement with acoustic theory and the results from the TMM models.
- For details refer to Mr. Marderness RPI Thesis
 (www.ewp.rpi.edu/~ernesto/SPR.html) or contact him directly at marderness2@sbcglobal.net